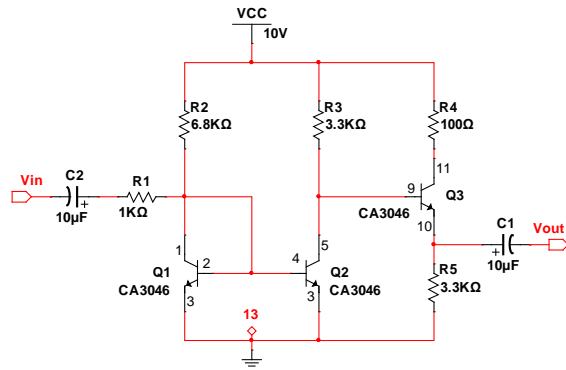


BEE 332 Lab 4
Multistage amplifiers
Spring 2017

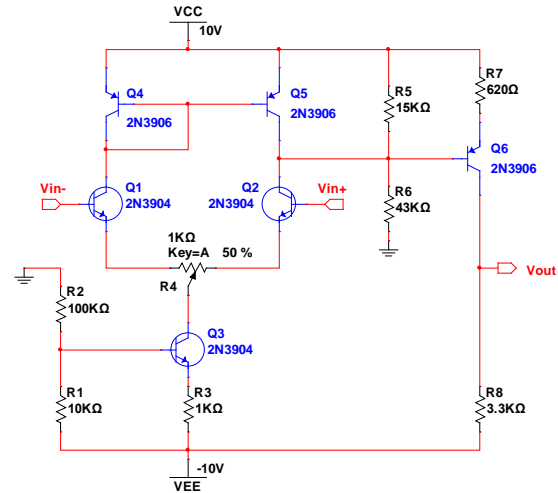
Nicole Hamilton

<https://faculty.washington.edu/kd1uj>

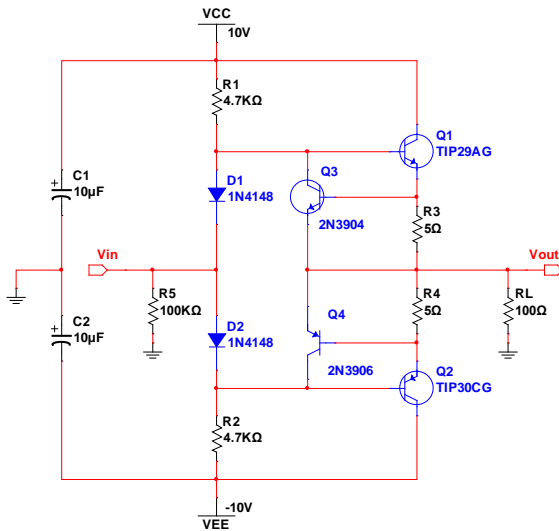
Four circuits



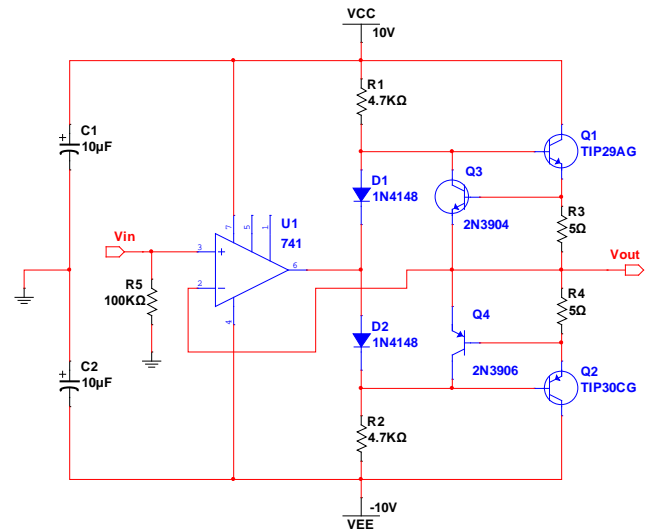
Wideband CE-EF amplifier.



A simple opamp.



Complementary class AB output stage.

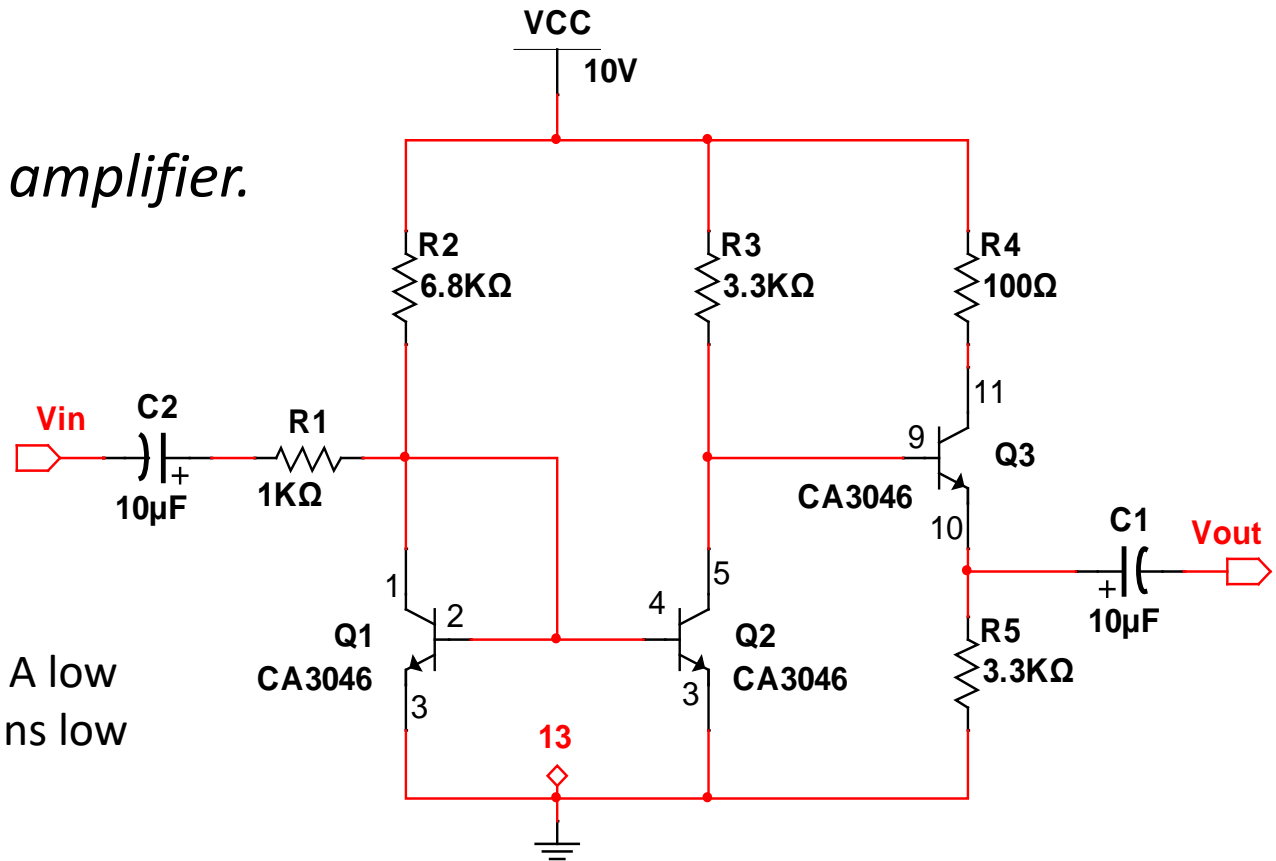


Multi-stage amplifier with feedback.

Wideband CE-EF amplifier.

A_v for a CE circuit is proportional to RC . A low resistance load means low A_v .

One solution is a second emitter follower stage, which offers only unity A_v , but $A_i = \beta + 1$

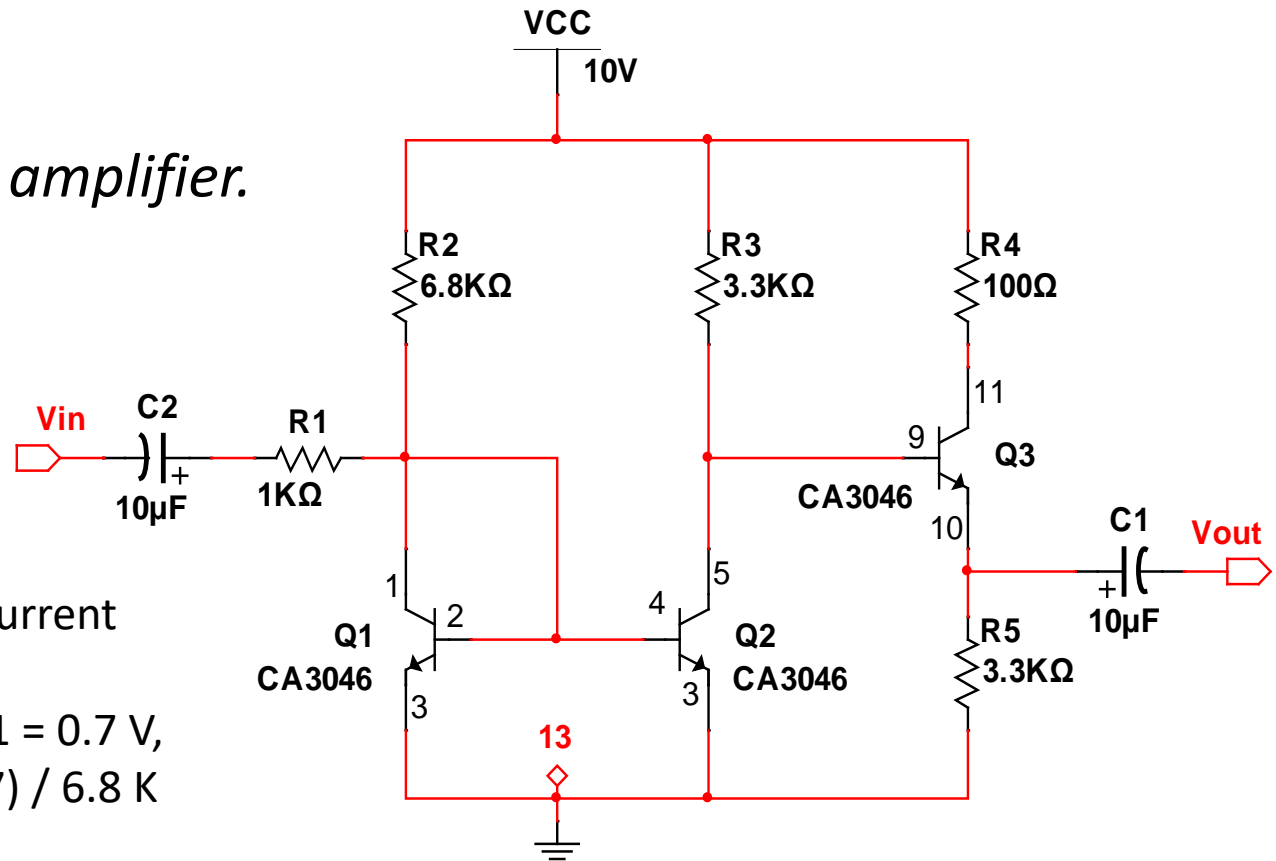


The Q1-Q2 pair is a current mirror, used here to bias Q2..

Whatever the value of I_{C1} , $I_{C2} = I_{C1}$.

$A_v \approx R3/R1$.

Wideband CE-EF amplifier.



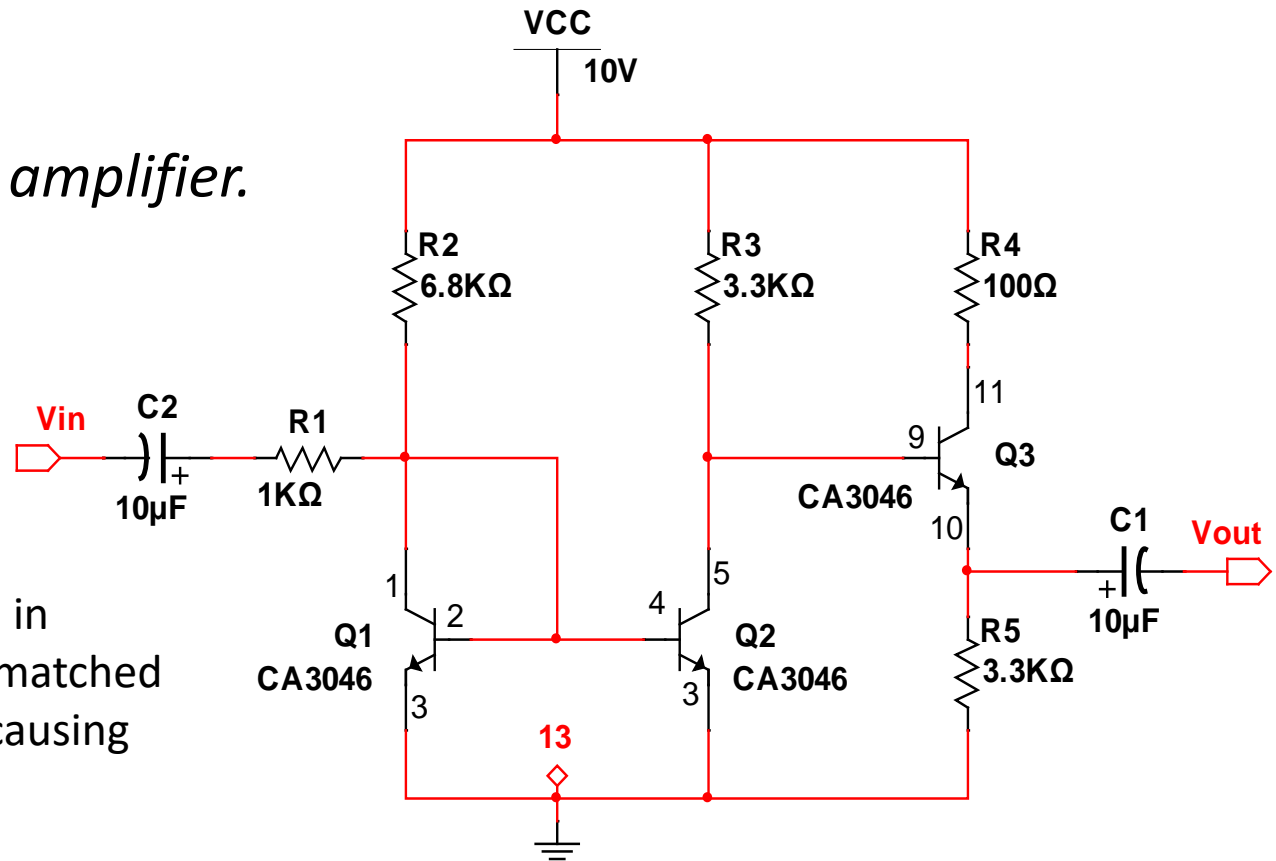
Q1 and Q2 form a current mirror.

With expected $V_{CE1} = 0.7 \text{ V}$,
 $I_{ref} = I_{R2} = (10 - 0.7) / 6.8 \text{ K}$
 $= 1.4 \text{ mA}$.

Assuming $I_{ref} \cong I_{C1}$, I_{R3} will
be about the same,
meaning $V_{B3} = 10 - 3.3 \text{ K} * 1.4 \text{ mA} = 5.38 \text{ V}$.

Quiescent V_{E3} should be
about $5.4 - 0.7 = 4.7 \text{ V}$.

Wideband CE-EF amplifier.



Both Q1 and Q2 are in forward active and matched with $V_{BE1} = V_{BE2}$, causing $I_{C1} = I_{C2}$.

If we inject a small additional current into I_{C1} , it will be matched in I_{C2} .

Since V_{BE} can be assumed constant at 0.7 V, we can ignore $R2$.

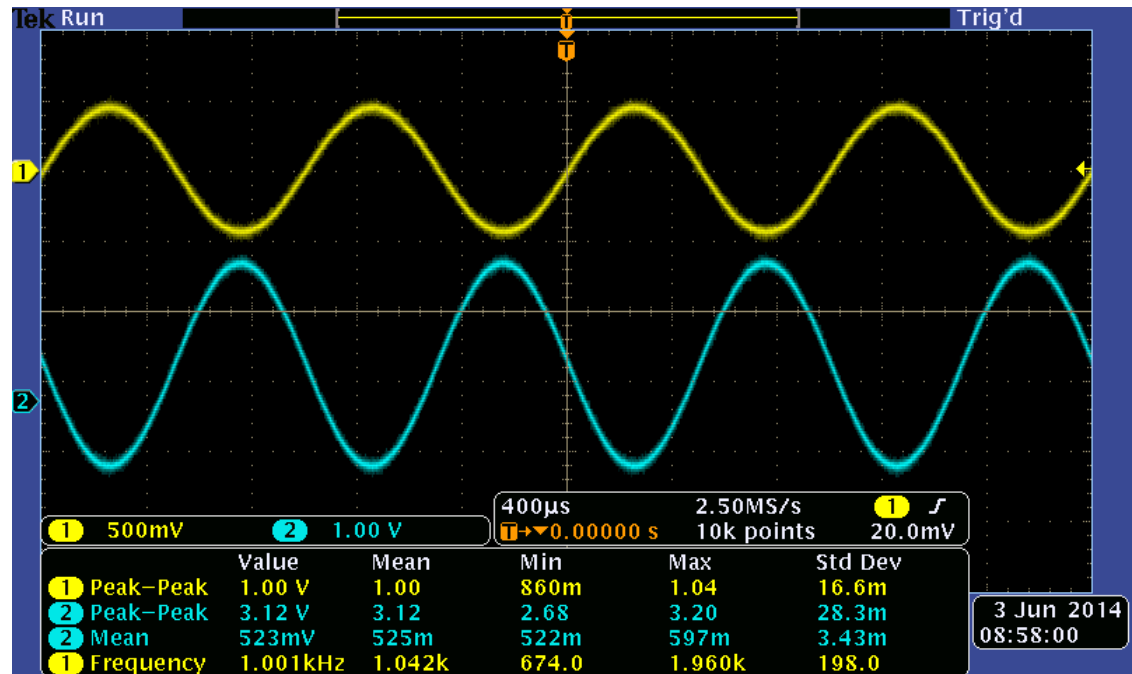
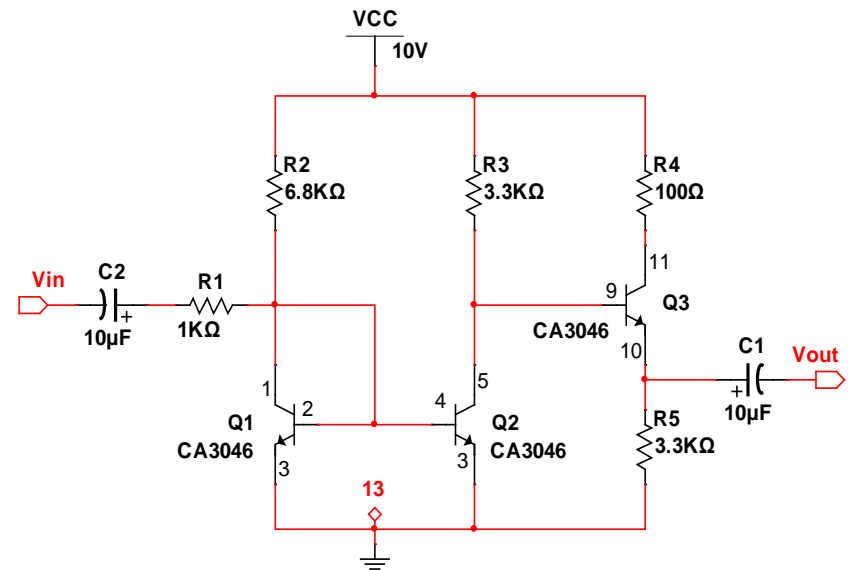
$$\Delta I_{ref} = \frac{\Delta V_{in}}{R1} \cong \Delta I_{C1} = \Delta I_{C2} \cong \Delta I_{R3}$$

$$\Delta V_{C2} = -R3 * \Delta I_{R3} = -R3 \left(\frac{\Delta V_{in}}{R1} \right) = - \left(\frac{R3}{R1} \right) \Delta V_{in}$$

$$A_v = \frac{\Delta V_{C2}}{\Delta V_{in}} = - \frac{R3}{R1}$$

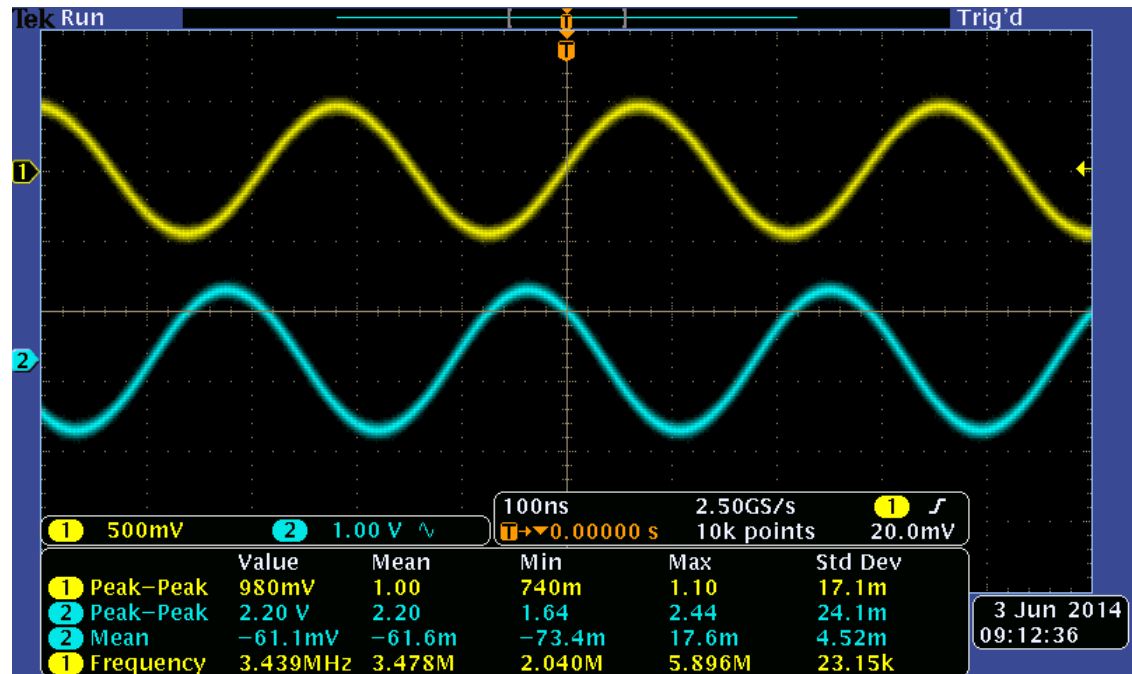
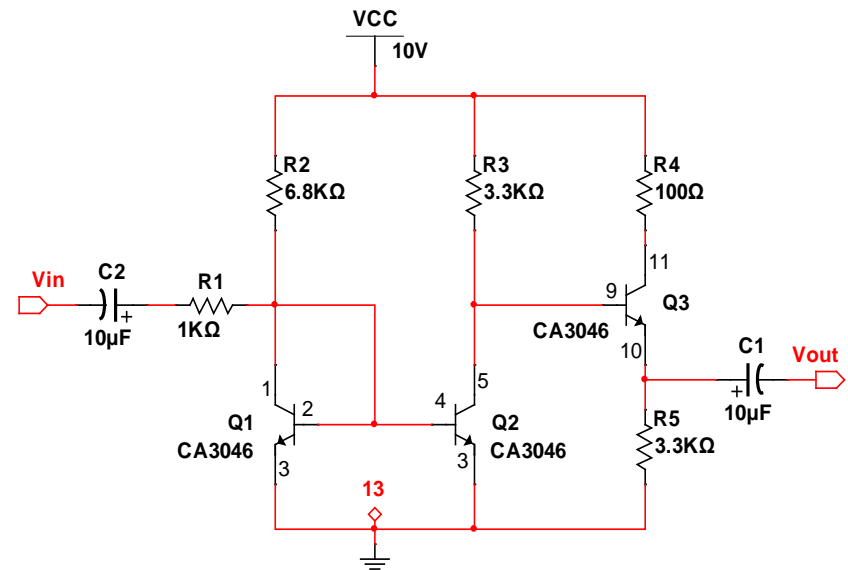
Measurements: Gain

1. Set $V_{in} = 1\text{ V}_{pp}$, 1.0 KHz sine wave, 0 V DC offset.
2. Capture an oscilloscope screenshot.
3. Calculate gain. For me, $A_v = 3.12$.



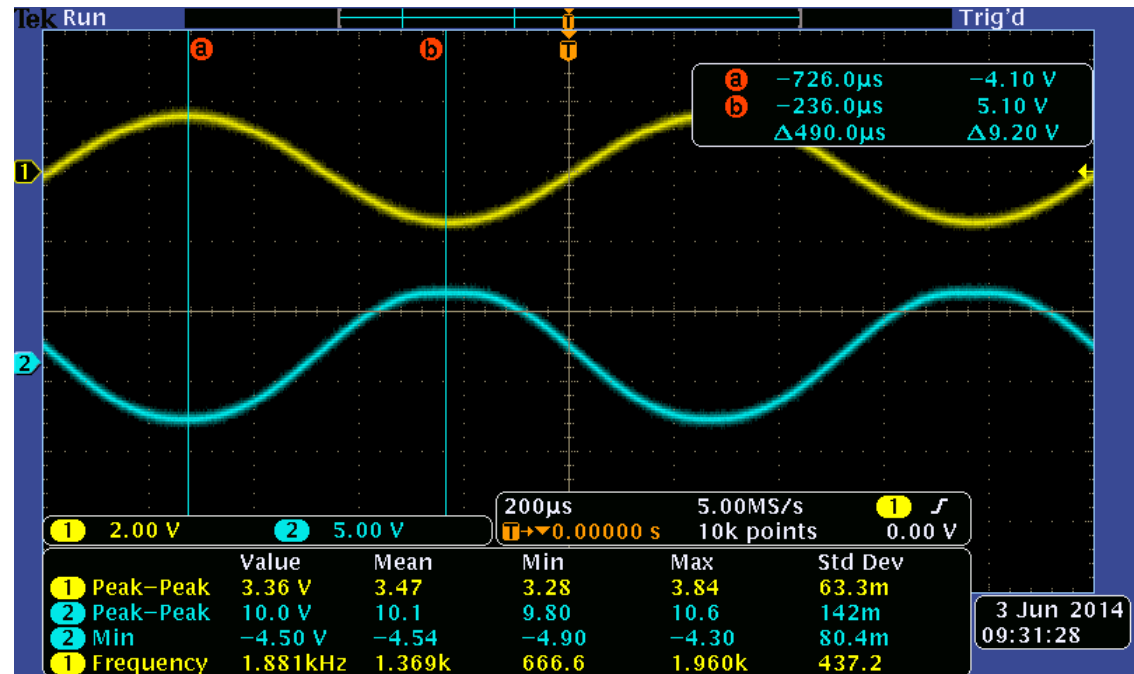
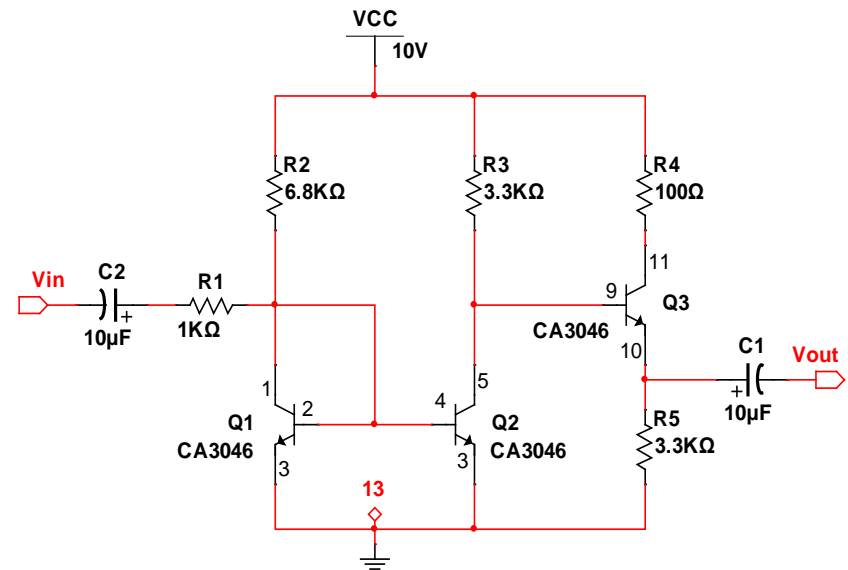
Measurements: Bandwidth

1. Increase frequency until A_v has fallen by 3 dB.
2. Capture an oscilloscope screenshot.
3. For me, $A_v = 2.20$ at 3.5 MHz.



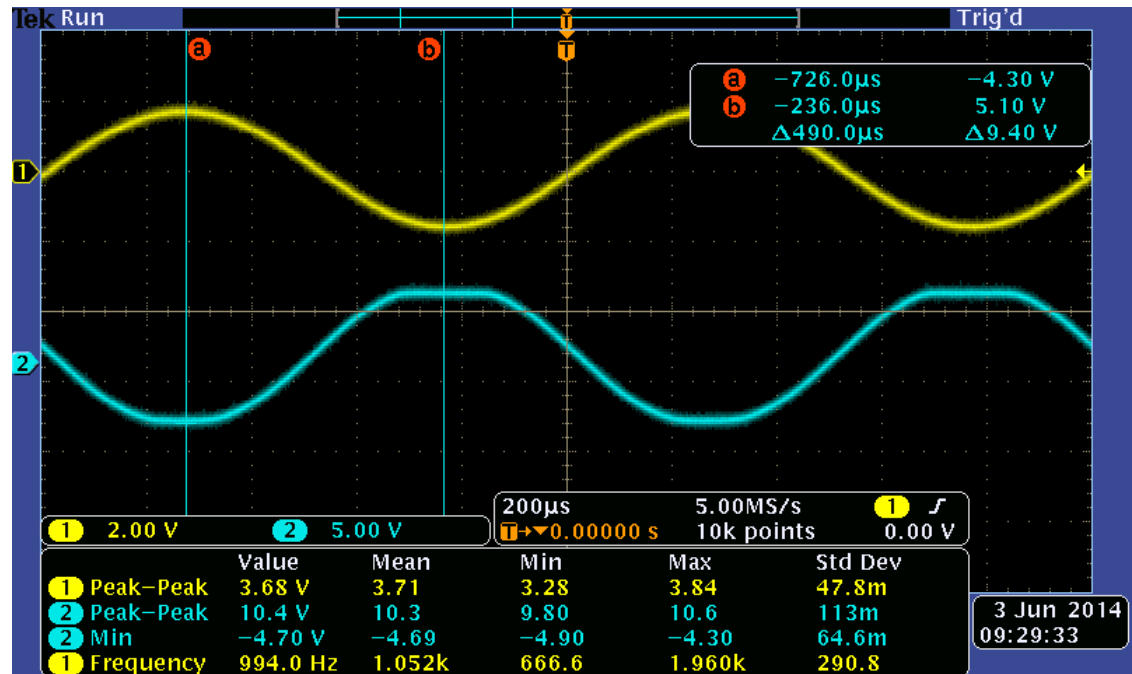
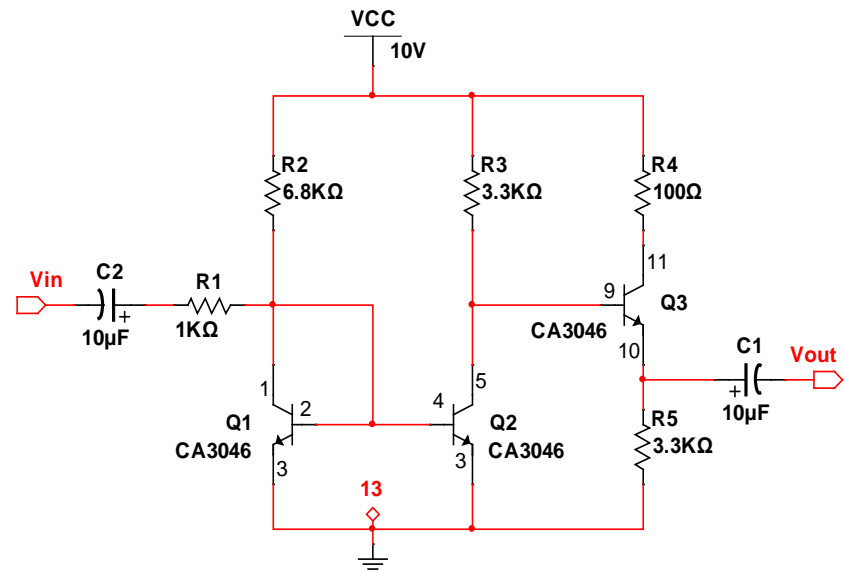
Measurements: Onset of clipping

1. Set $V_{in} = 1 \text{ Vpp}$, 1.0 KHz sine wave, 0 V DC offset .
2. Increase amplitude until onset of clipping.
3. Capture an oscilloscope screenshot.
4. For me, $V_{in} = 3.47 \text{ Vpp}$ and $V_{out} = 10.1 \text{ Vpp}$.



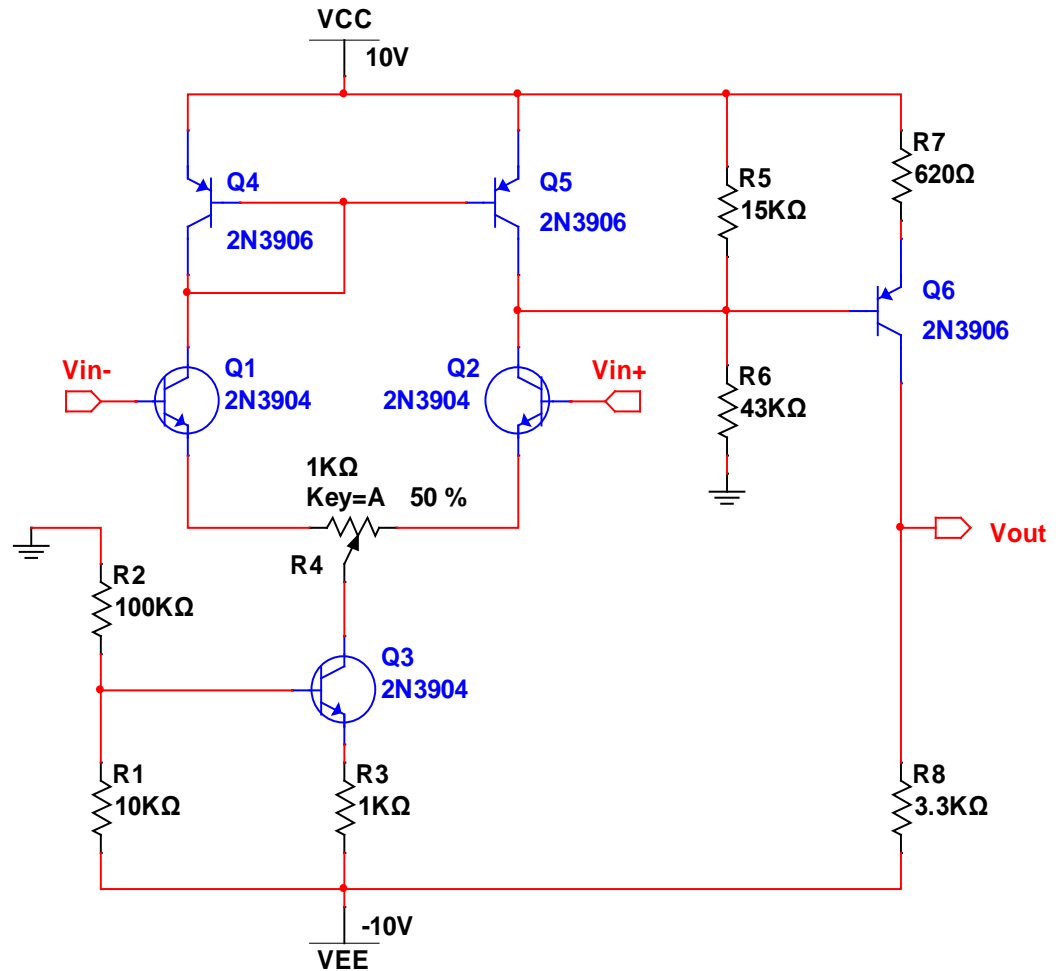
Measurements: Clipping both peaks

1. Increase amplitude until clipping on both peaks.
2. Capture an oscilloscope screenshot.
3. For me, $V_{in} = 3.71$ Vpp and $V_{out} = 10.3$ Vpp.



A simple opamp.

An active load usually refers to the use of a transistor as the output load for a common-emitter stage, greatly increasing the voltage gain since the collector resistance for the CE amplifier stage is now the output resistance of the active load transistor.

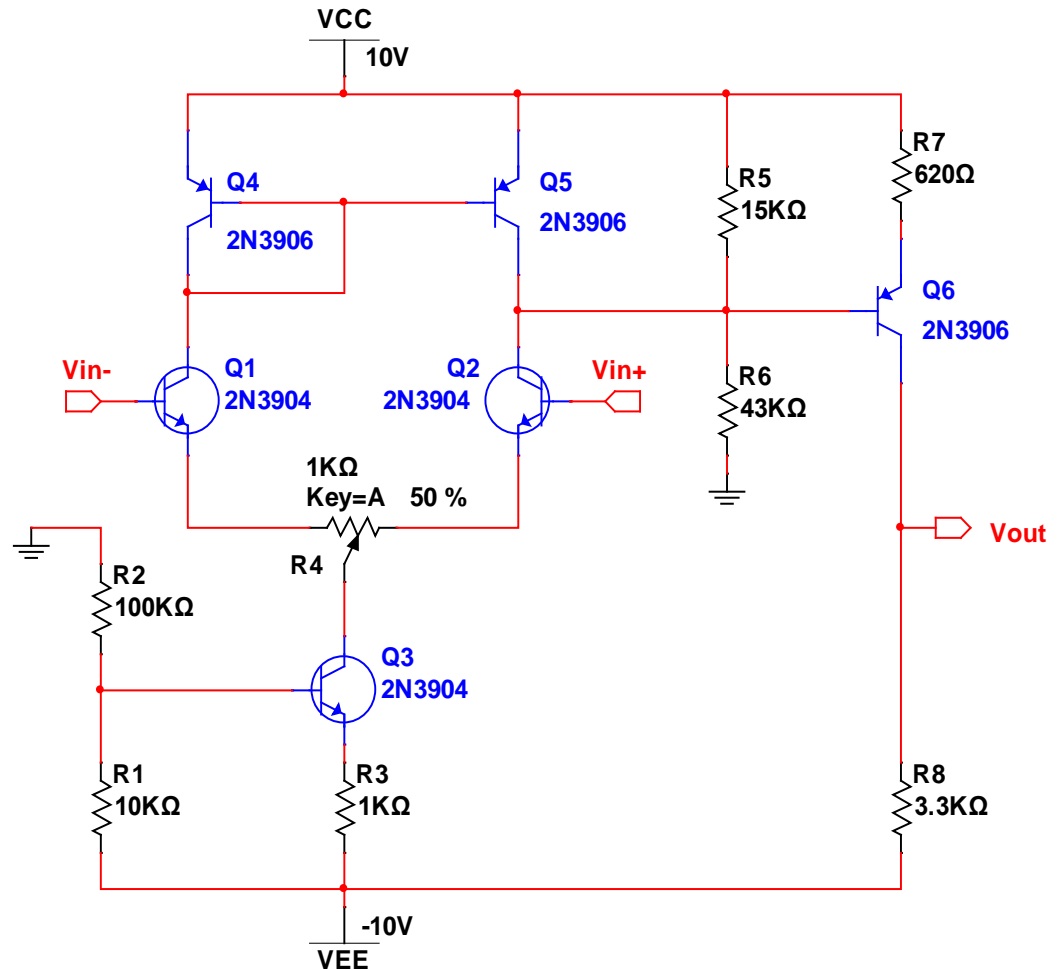


A simple opamp.

Q3 provides a current source for the differential pair.

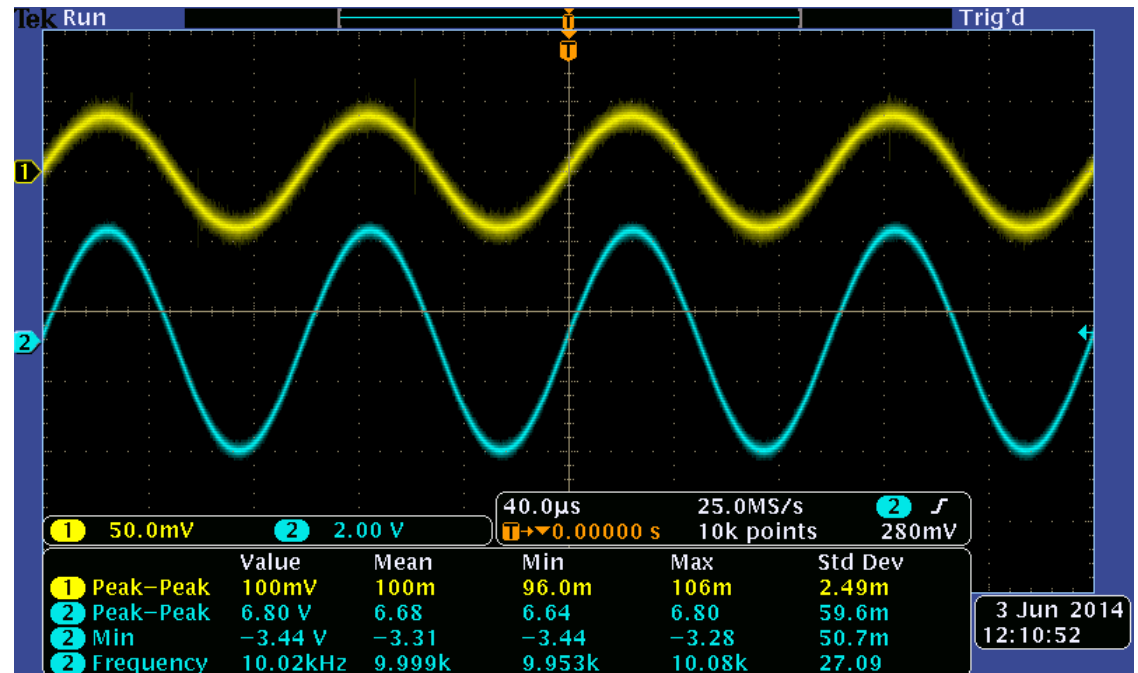
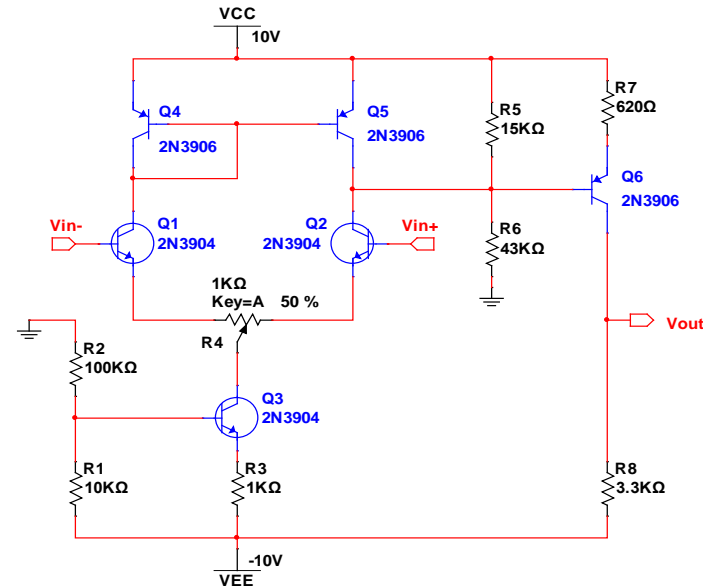
Q6 is a simple PNP CE stage.

R4 is an optional trimpot to allow the differential pair to be balanced so the output is zero when the differential input is zero. But it lowers the gain.



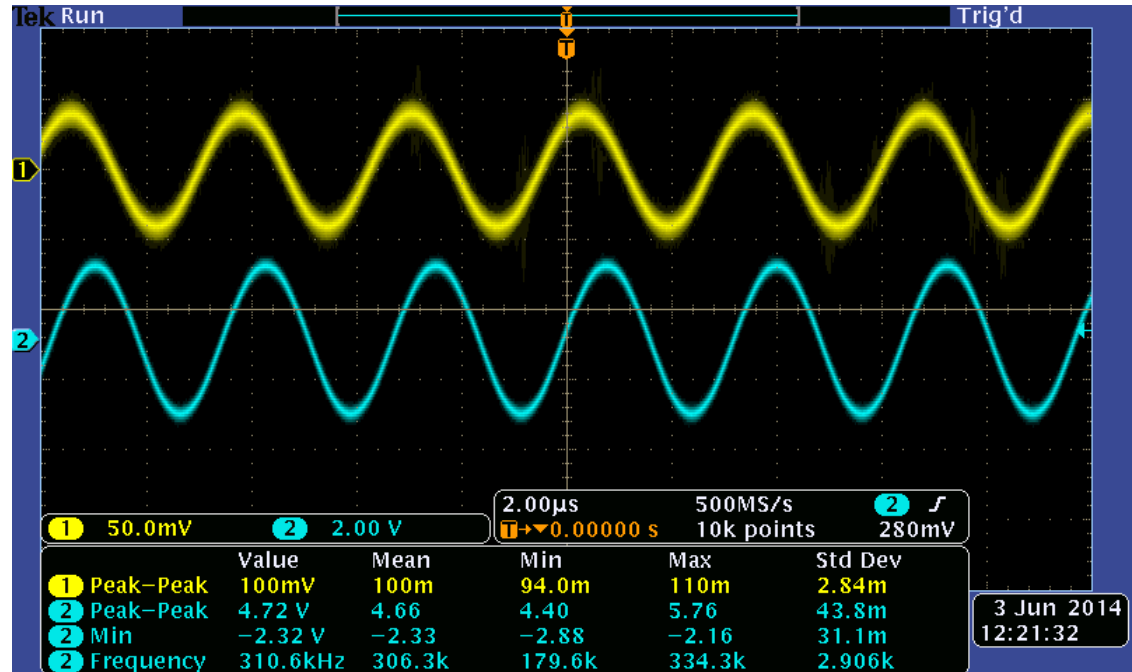
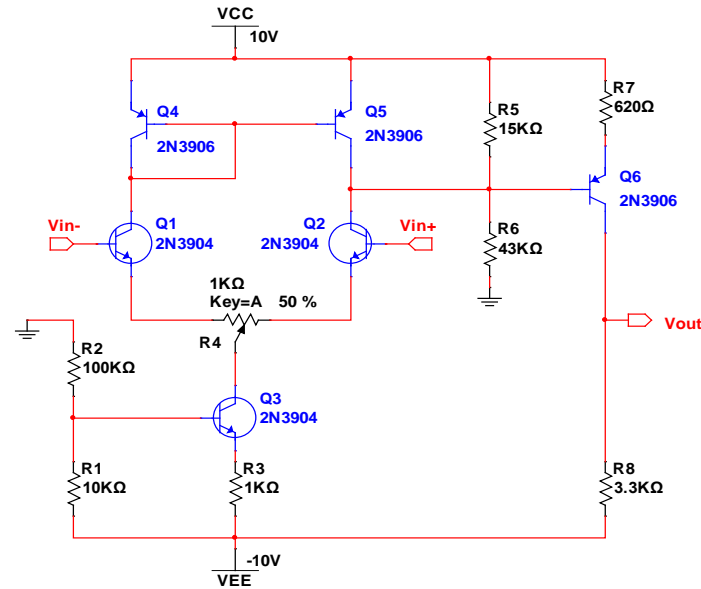
Measurements: Gain

1. Set $V_{in} = 100 \text{ mVpp}$, 1.0 KHz sine wave, 0 V DC offset.
2. Capture an oscilloscope screenshot.
3. Calculate gain. For me (at 10 KHz), $A_v = 66.8$.
4. $A_v(\text{dB}) = 20 \log_{10}(66.8) = 36.5 \text{ dB}$.



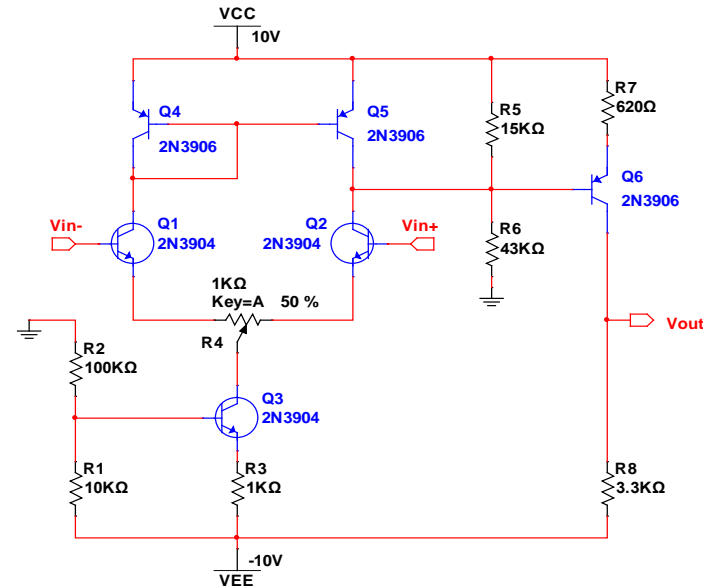
Measurements: Bandwidth

1. Increase the frequency of V_{in+} until A_v has fallen by 3 dB.
2. Capture an oscilloscope screenshot.
3. For me, $A_v = .7071 * 66.8 = 47.2$.
Shown here, $A_v = 47.2$ at 310.6 KHz.

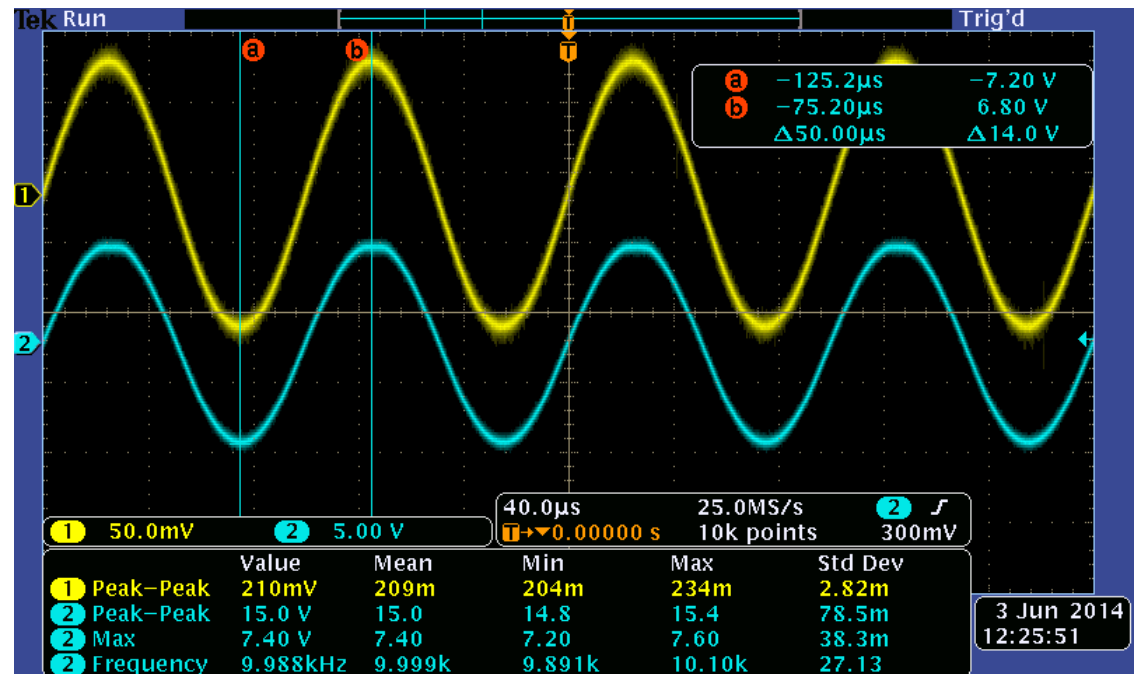


Measurements: Onset of clipping

1. Increase amplitude of V_{in} until onset of clipping.
2. Capture an oscilloscope screenshot.
3. For me, $V_{in} = 209 \text{ mVpp}$.
4. V_{out} is clipping between 6.80 V (cursor) and 7.40 V (Max).

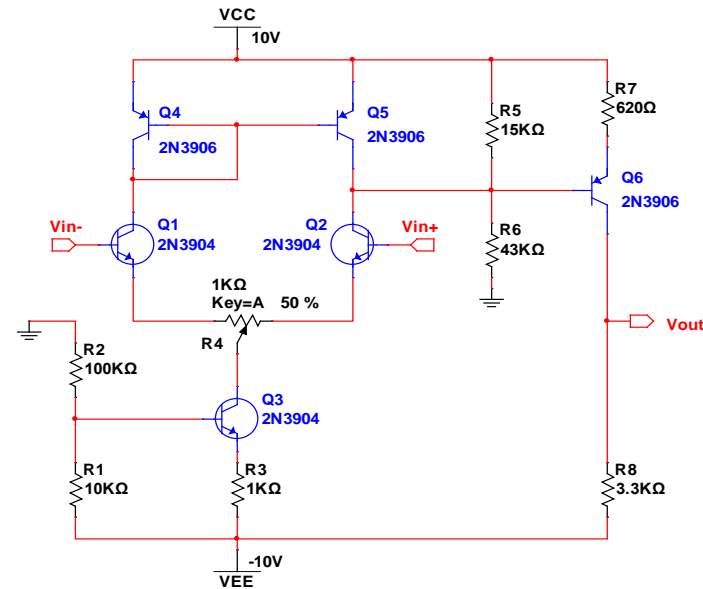


Clipping on the top happens when Q6 saturates.

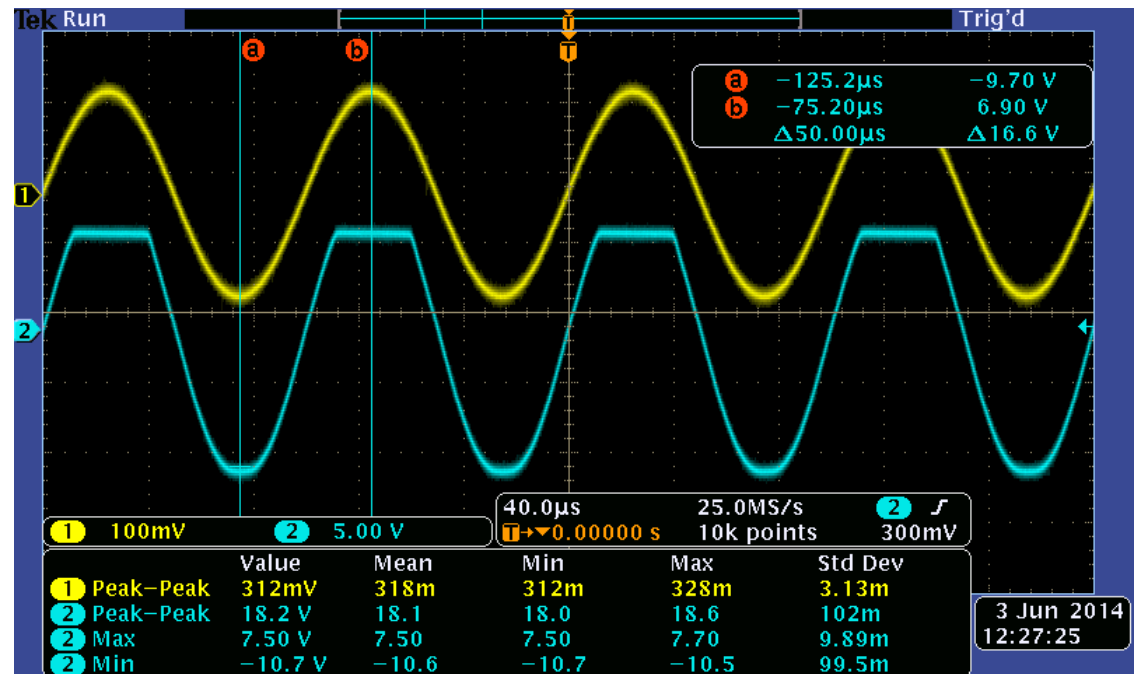


Measurements: Clipping both peaks

1. Increase amplitude of V_{in} until clipping both peaks.
2. Capture an oscilloscope screenshot.
3. For me, $V_{in} = 318 \text{ mVpp}$.
4. V_{out} tops are clipping between 6.90 V (cursors) and 7.50 V (Max).
5. Bottoms are clipping between -9.70 V (cursors) and -10.6 V (Min).



Clipping on the bottom happens when Q6 enters cutoff.



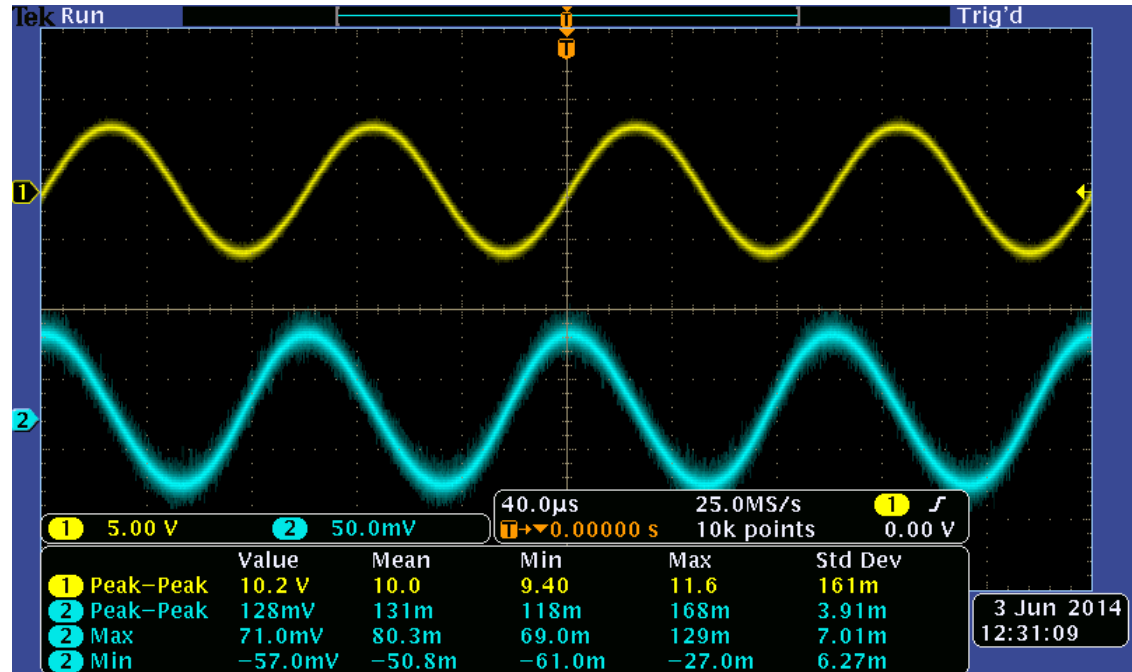
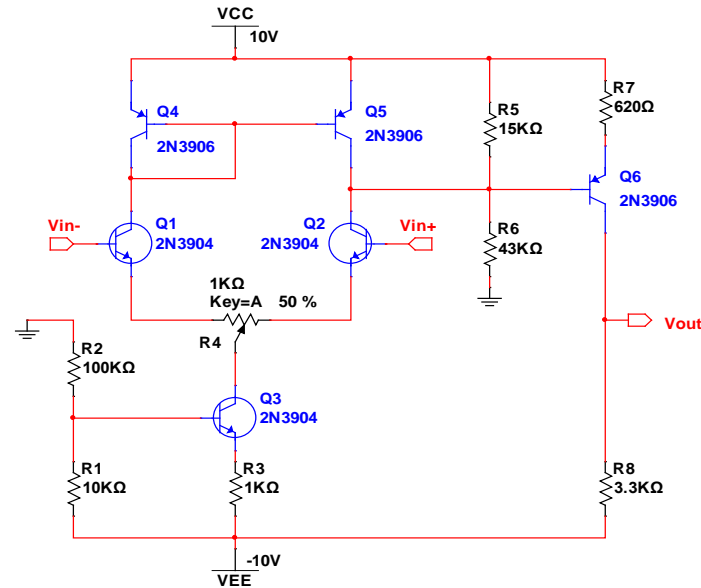
Measurements: Common mode

1. Set $V_{in-} = V_{in+} = 10 \text{ Vpp}$, 1.0 KHz sine wave, 0 V DC offset.
2. Shown here, $A_v(\text{common mode}) = 131 \text{ mVpp} / 10.0 \text{ Vpp} = .013$.
3. $A_v(\text{cm})\text{dB} = 20 \log_{10}(A_v) = -37.7 \text{ dB}$

Common mode rejection ratio (CMRR)

$$= A_v(\text{dm in dB}) - A_v(\text{cm in dB})$$

$$= 36.5 - (-37.7) = 74.2 \text{ dB}$$



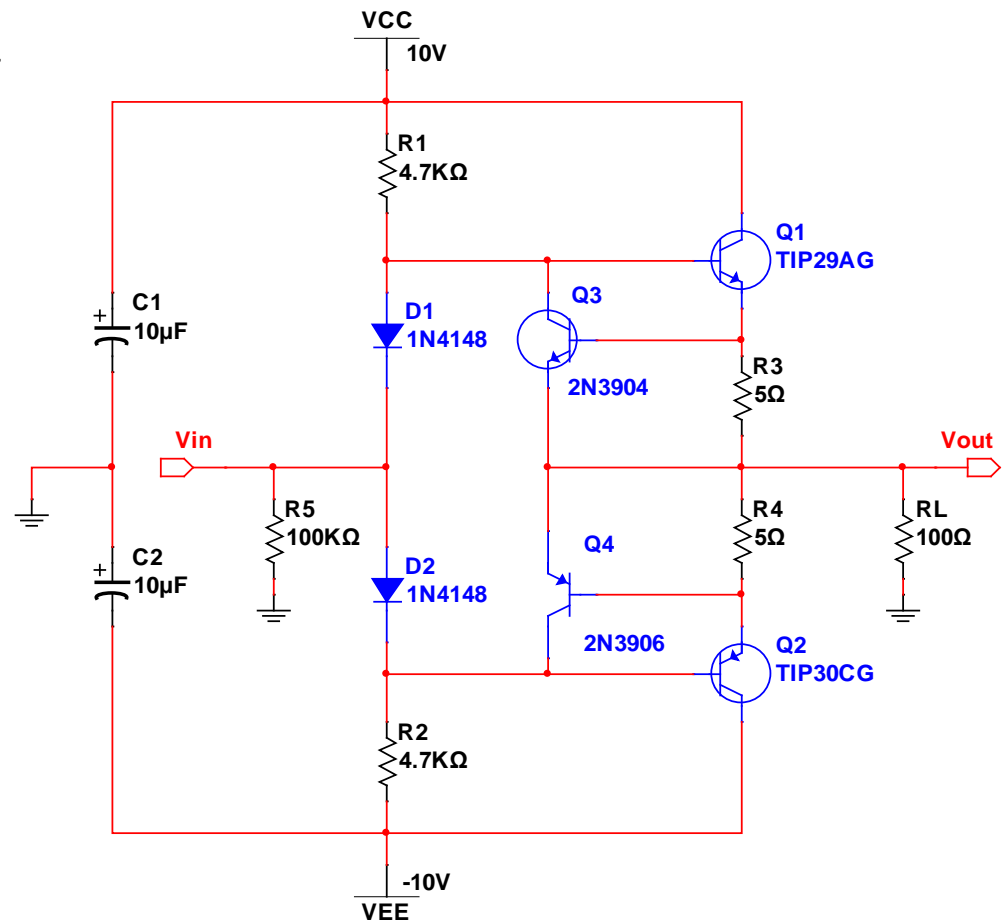
Complementary AB output stage.

The quiescent power dissipated in a transistor = $I_C * V_{CE}$ at the Q-point.

One way to reduce quiescent power is by using two a complementary pair or NPN and PNP transistors.

At the Q-point, both transistors are off. Q1 turns on when V_{in} is positive and Q2 turns on if V_{in} is negative.

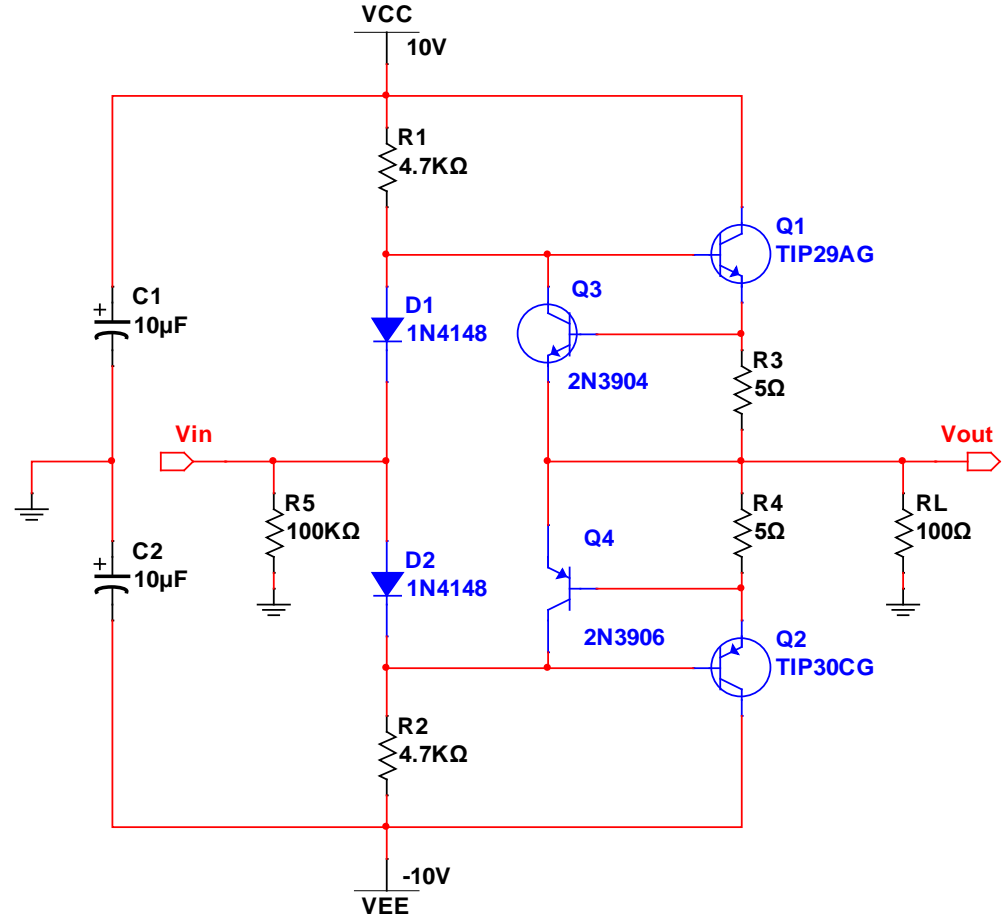
This is called class AB operation.



Use heat sinks on Q1 and Q2.

Short-circuit protection.

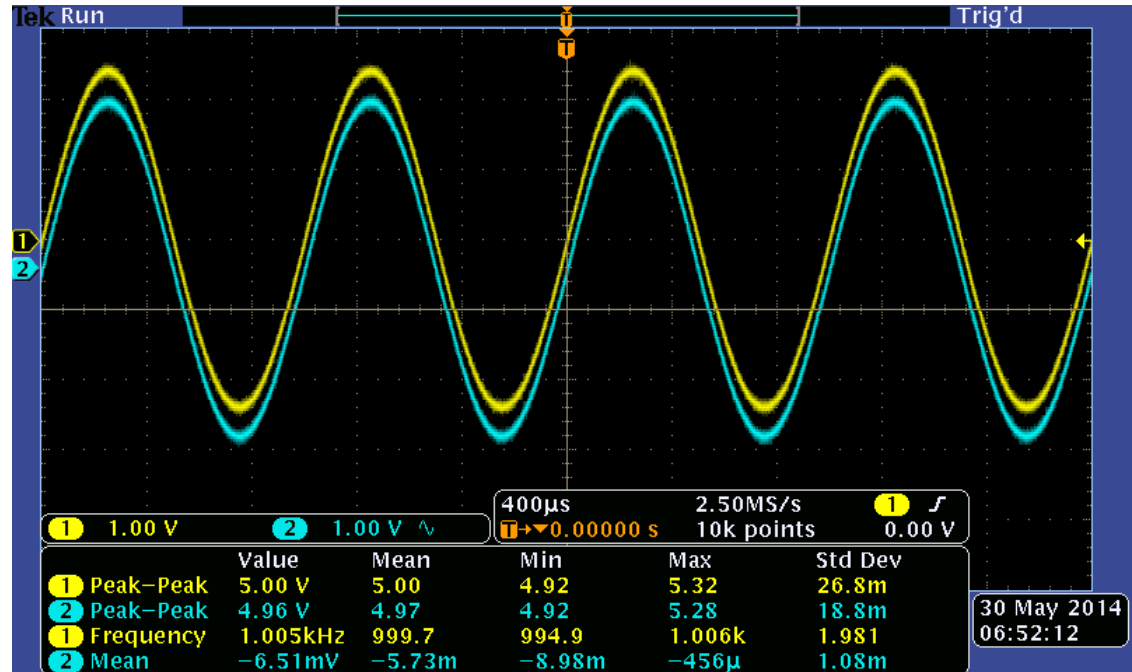
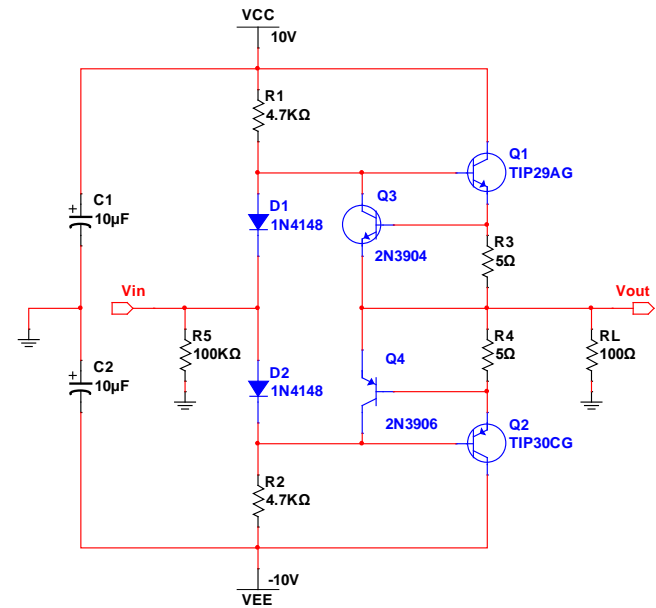
Q3 and Q4 provide short-circuit protection. When the voltage drop across either R3 or R4 > 0.7 V, either Q3 or Q4 will turn on, dropping the base voltages VB1 or VB2, cutting them off.



Use heat sinks on Q1 and Q2.

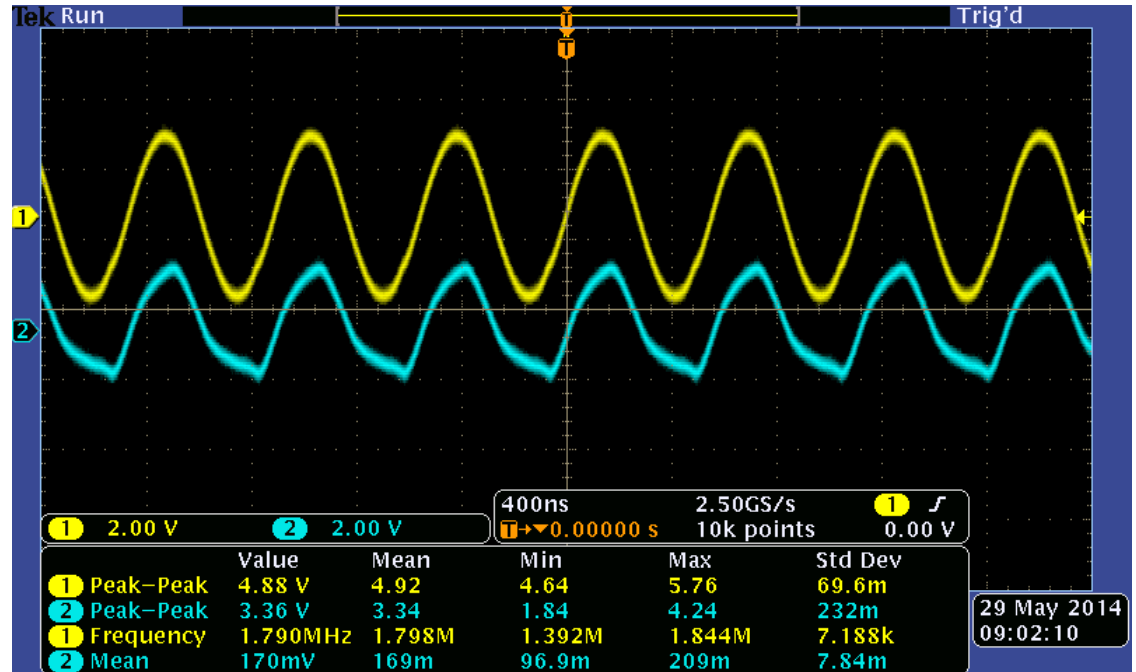
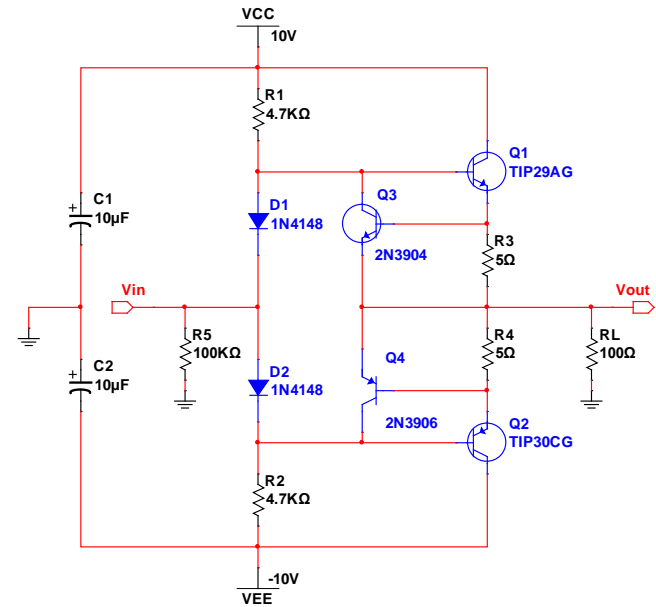
Measurements: Gain

1. Set $V_{in} = 5.0$ Vpp, 1.0 kHz. Capture a screenshot and calculate A_v .
2. $A_v = 4.97 / 5.00 = .99$, just under unity, and non-inverting.
3. V_{out} has only a -5.7 mV DC offset.



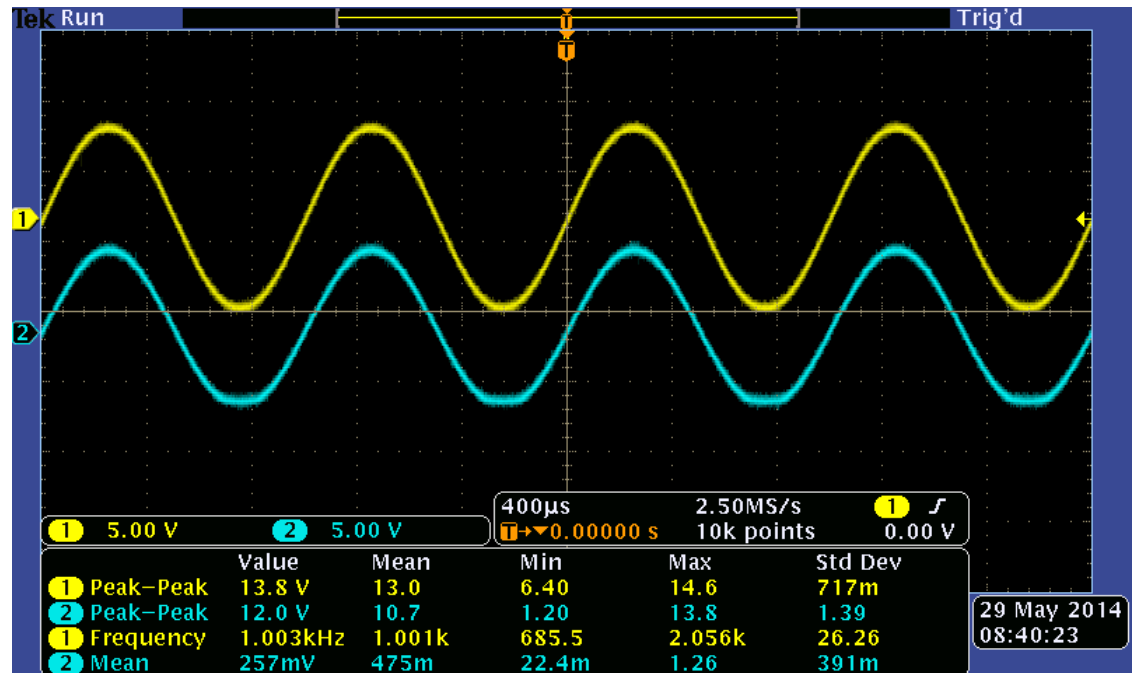
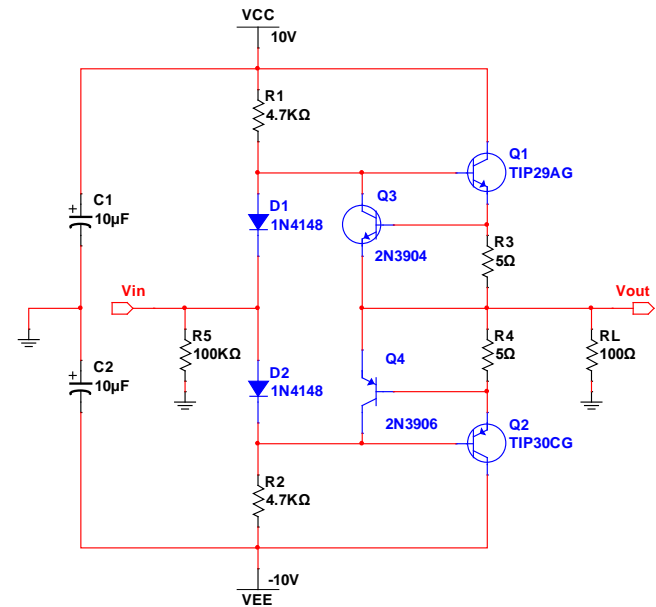
Measurements: Bandwidth

1. Find the 3 dB point. For my circuit, this would be where $A_v = .7071 * .99 = .70$.
2. Shown here, $A_v = 3.34 / 4.92 = .68$ at 1.8 MHz.
3. But note the distortion.



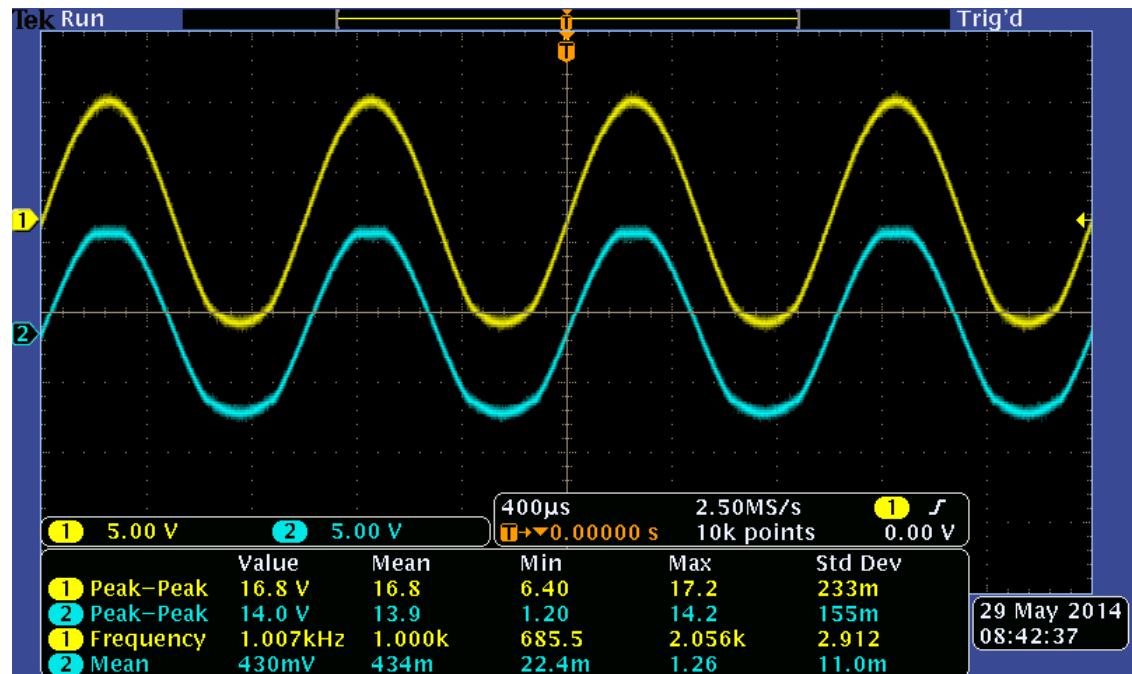
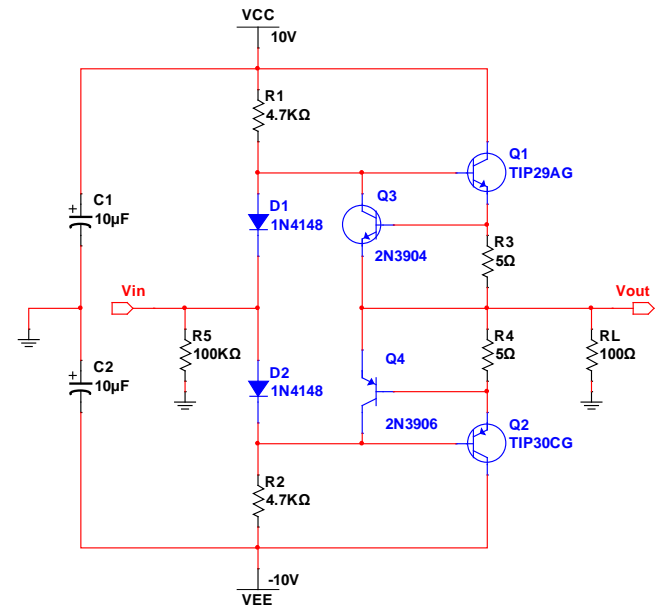
Measurements: Onset of clipping

1. Reset V_{in} to 1.0 KHz and increase the amplitude until V_{out} begins clipping on either peak.
2. For me, clipping on negative peaks is at $V_{out} = 10.7$ Vpp.



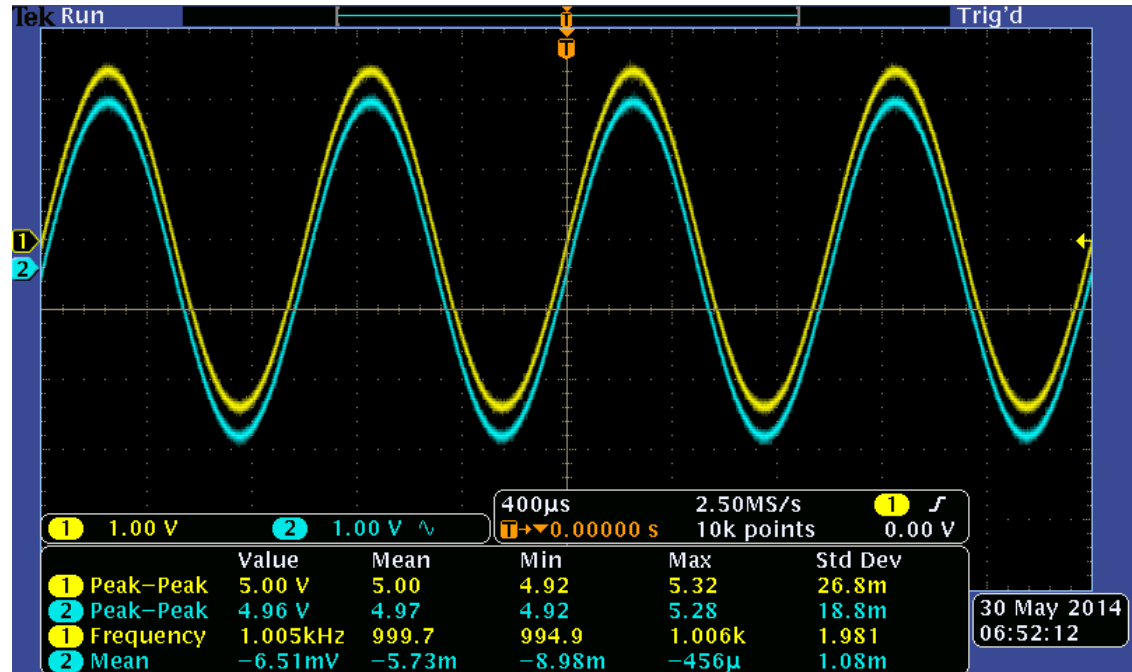
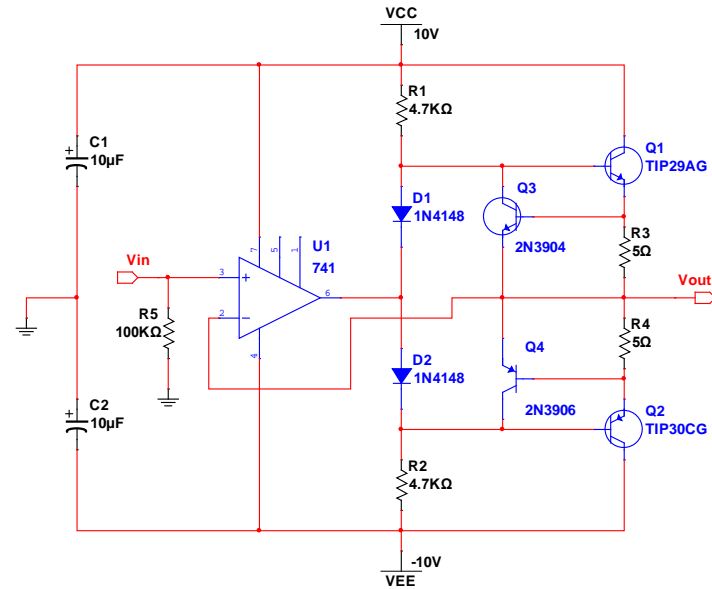
Measurements: Clipping both peaks

1. Continue increasing the amplitude of V_{in} until V_{out} begins clipping on the other peak.
2. For me, clipping on both peaks occurs at $V_{out} = 13.9$ Vpp..



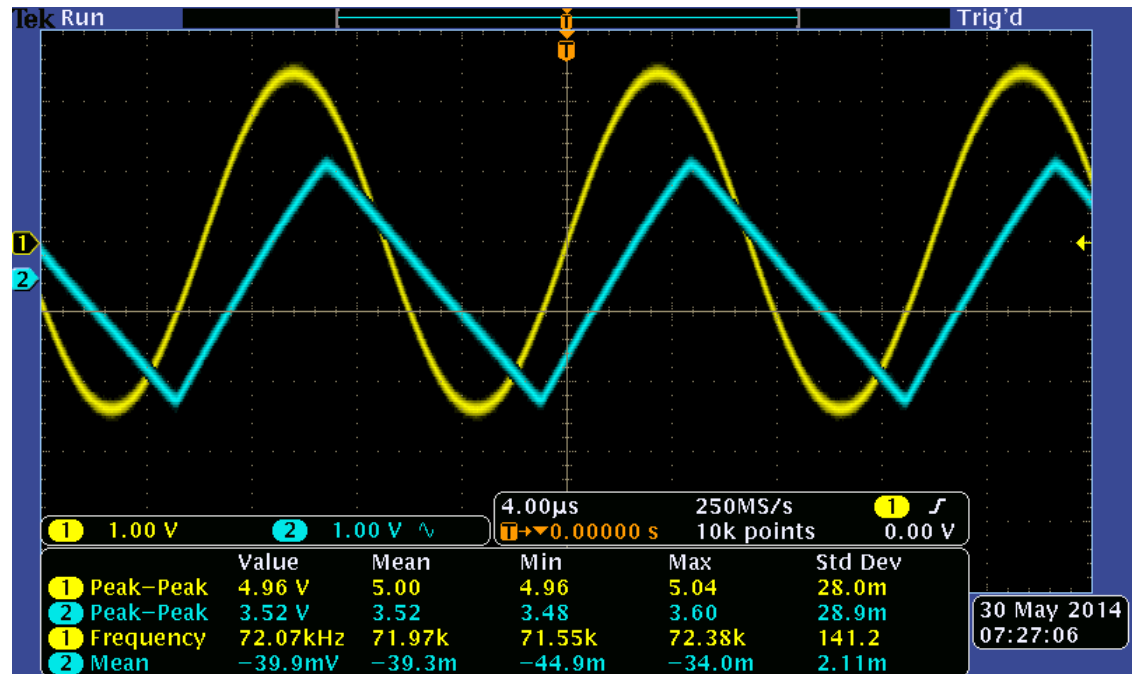
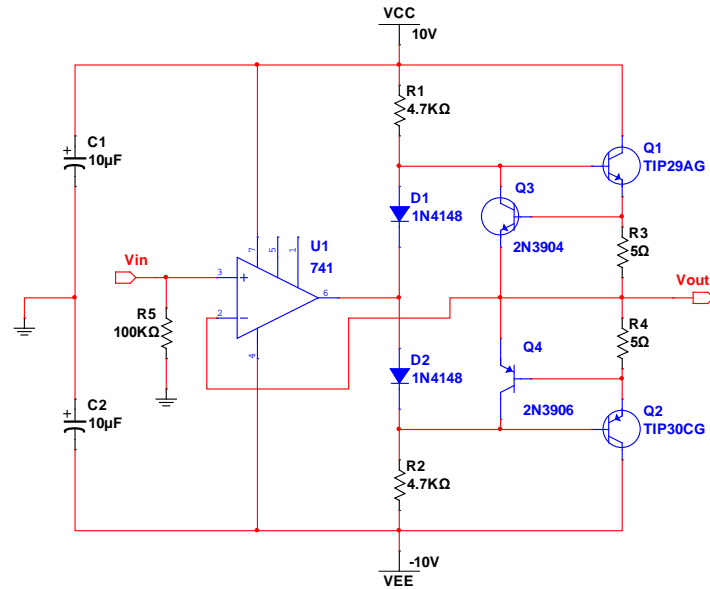
Measurements: Gain

1. Set $V_{in} = 5.0$ Vpp, 1.0 kHz. Capture a screenshot and calculate A_v .
2. $A_v = 4.97 / 5.00 = .99$, just under unity, and non-inverting.
3. V_{out} has only a -5.7 mV DC offset.



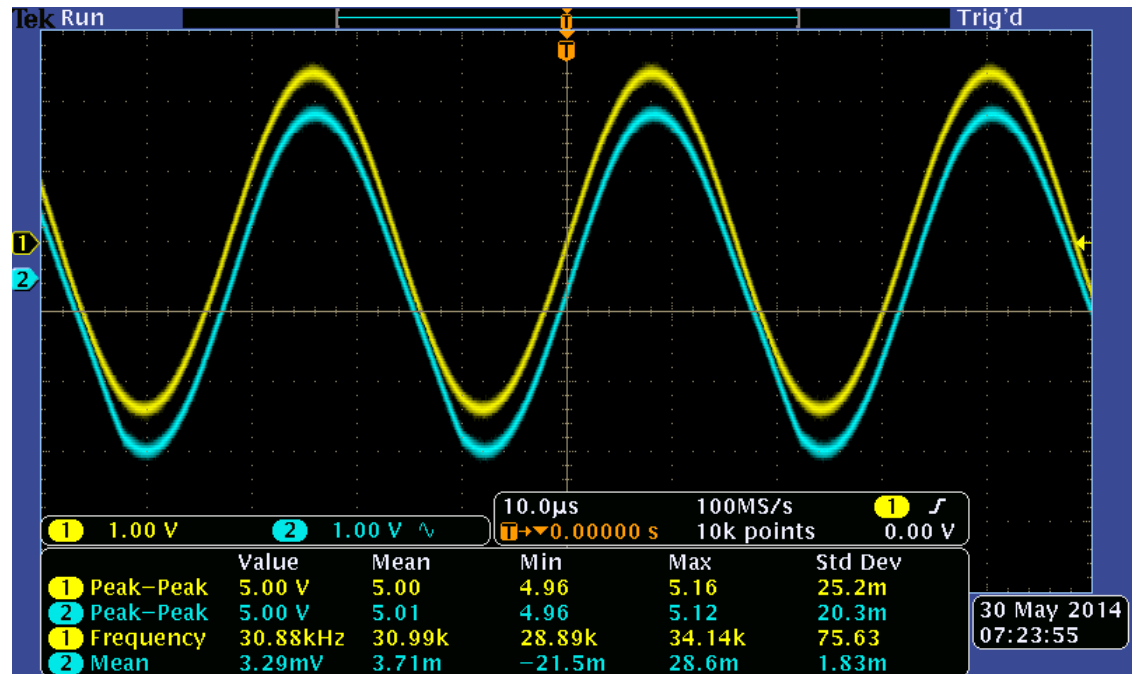
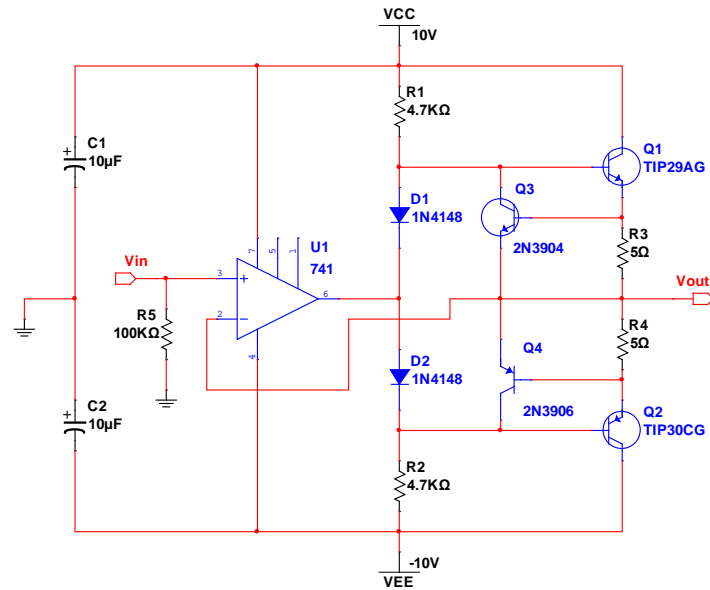
Measurements: Bandwidth

1. Find 3 dB point.
2. Shown here, $A_v = 3.52 / 5.00 = .704$ at 72 KHz.
3. But note the distortion. The output is almost a triangle because we've hit the opamp's slew rate.



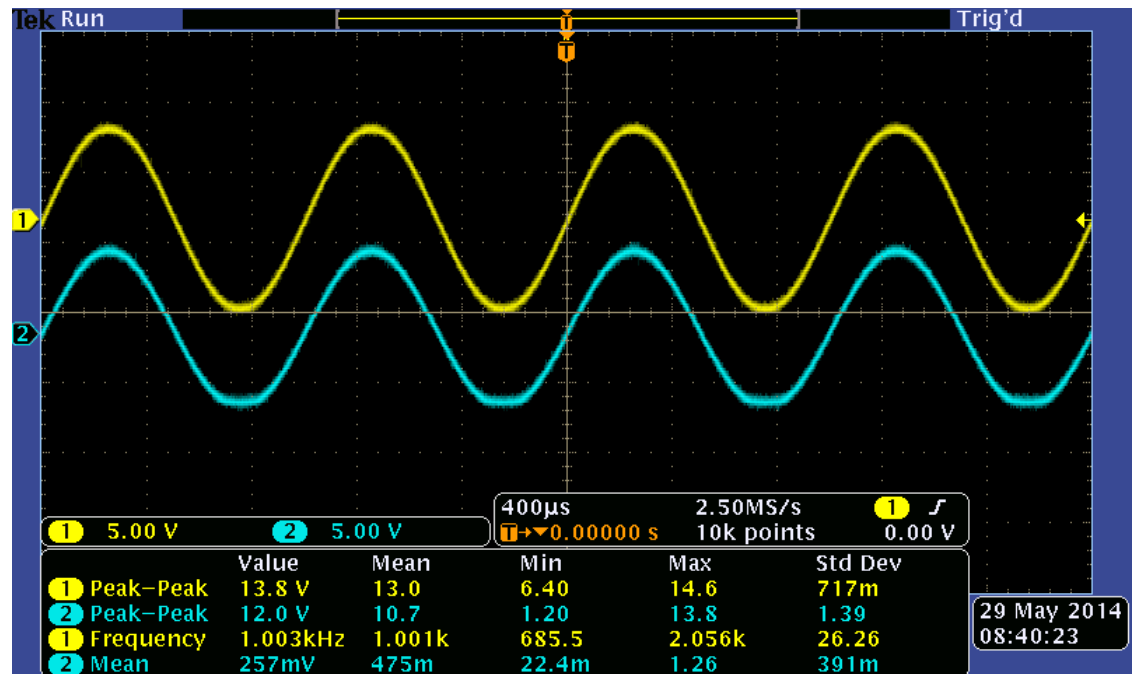
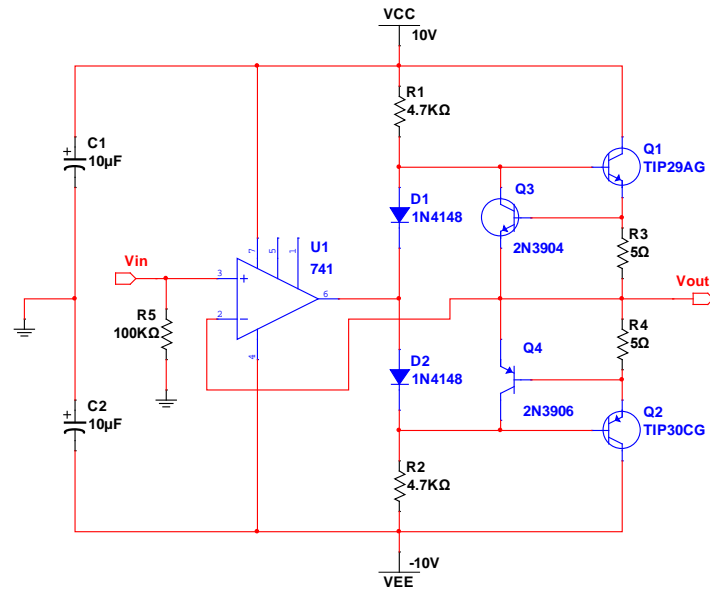
Onset of slew rate limitation.
(Not required.)

About 31 KHz for $V_{in} = 5.0$ Vpp.



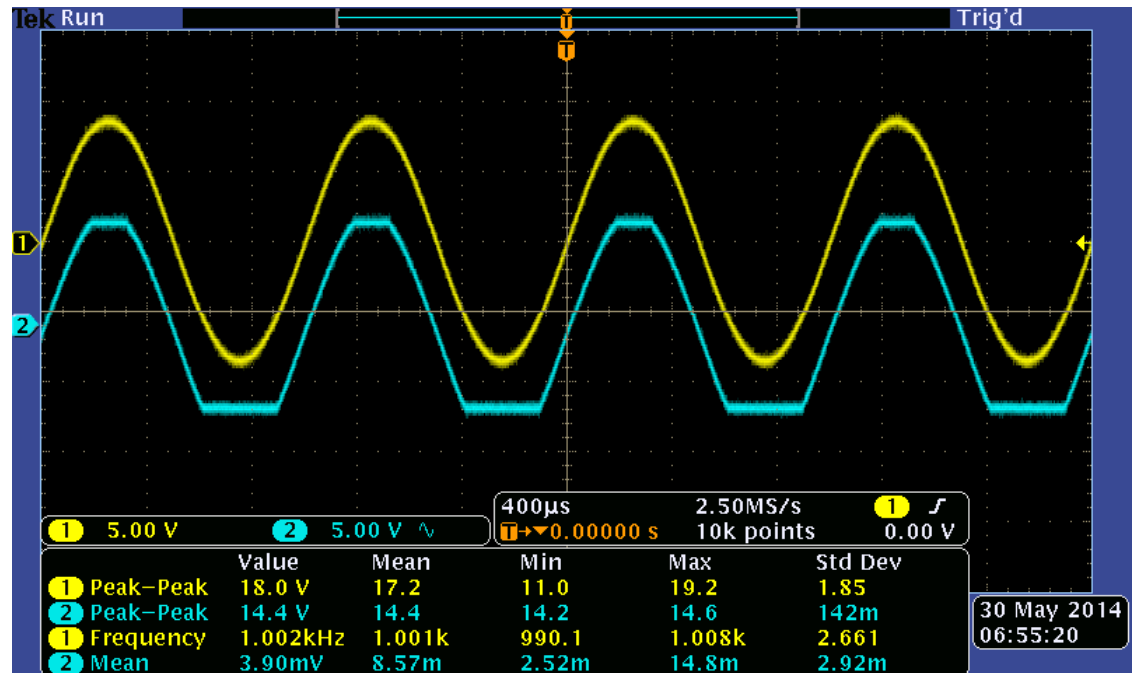
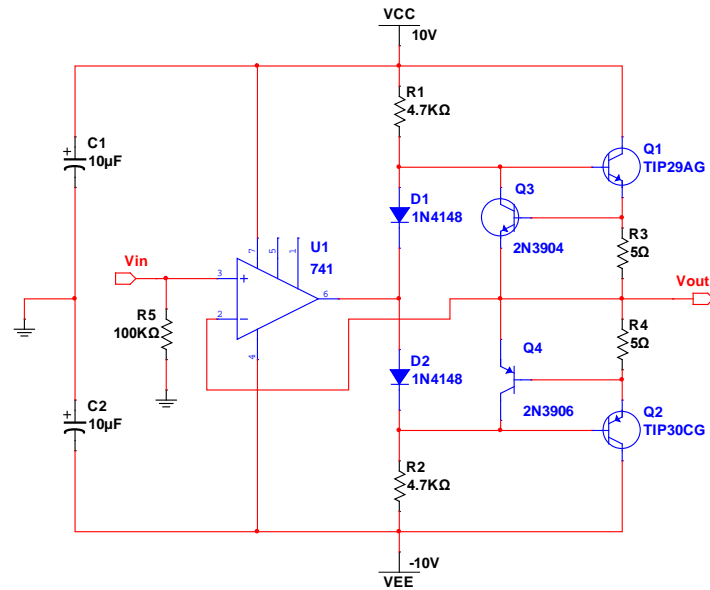
Measurements: Onset of clipping

1. Increase V_{in} until clipping begins.
2. Shown here, it's clipping negative at $V_{in} = 13 \text{ Vpp}$.



Measurements: Clipping both peaks

1. Increase V_{in} until clipping begins.
2. Shown here, it's clipping both peaks happens at $V_{in} = 17 \text{ Vpp}$.



My results, comparing with and without the opamp front-end and feedback loop.

	Without opamp	With opamp
Vin Initial clipping	10.7 Vpp	13 Vpp
Vin Clipping both peaks	13.9 Vpp	17 Vpp
Bandwidth	1.8 MHz	72 KHz